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Development of a Process Based on Coagulation of polyurethane in Aqueous Solution for Manufacturing Leather-like Products

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Multilayer synthetic leather-like textiles are traditionally manufactured by using dimethylformamide as a diluent via polymeric polyurethane coating and coagulation processes. Unfortunately, this process has a strong environ-mental impact since it encompass a complex and polluting grinding process to separate dimethylformamide from water. Furthermore, this compound was proved harmful for both environment and textile practitioners' health. The aim of this work is to improve the state of the art in the production of leather-like fabrics through the devel-opment of an innovative process of coagulation of polyurethane in aqueous solution to replace the current highly polluting process that involves the use of dimethylformamide. The coagulation is obtained by means of an IR thermal fixing thus resulting in a completely eco compatible manufacturing process. The obtained quality of the manufactured synthetic leather, tested according to textile standards, is comparable to the one obtained by means of conventional processes.

Keywords: Leather-like, Fabrics, Manufacturing, Thermal Fixing, Polyurethane, Foaming Machine

1 Introduction and background

In recent years, the use of multilayer textile products obtained by coating and coagulation of polyure-thane polymers (PU) faced a growing interest in many markets due to the exceptional characteristics in terms of textile "hand" and appearance, similar to natural leather [1-3].

The typical production cycle of companies producing polyurethane coatings for creating leather-like products typically foresees, in many phases, the use and consumption of a nitrogenous organic compound called Dimethylformamide (DMF) as natural solvent of polyurethane polymers. As widely recognized, DMF is the amide of dimethylamine and formic acid. Its exact name is N,N-Dimethylformamide QP and its chemical formulation is (CH3)2NOH M.=73.10 CAS [68-12-2] EINECS 200-679-5 EEC 616-001-00-X.

Synthetic leather fabrics, which are used both for fashion products and for technical use, are manufactured with polyurethane in solution of dimethylformamide that is coagulated with water. Unfortunately, this process has a strong environmental impact since after the textile substrate is covered with polymeric materials it is necessary to separate DMF from water by means of a complex and polluting process [4]. Moreover, the use of DMF has harmful characteristics; it has long been known to be toxic to the liver, may cause abdominal pain, constipation, nausea and vomiting, headache, weakness, dizziness, skin problems,

and alcohol intolerance [5].

Other undesired properties that characterize DMF compounds are related to its physical properties: the vapours are heavier than air, so they can move at ground level and can form explosive mixtures with air. Therefore, in the event of a fire, NOx vapours can be formed. For these reasons, it is necessary that DMF does not pass through the discharge system in order to avoid soil and water contamination. Absorbent materials (General Panreac Absorbent, Kieselguhr, etc.), dry sand or soils are required to collect any leaks.

The new European Directive enacted the regulation 44/04 VOC (volatile organic compounds), thus imposing the application of the European Council Directive 2019/2020 of 20 June 2019 on the limitation of emissions of volatile organic compounds due to the use of organic solvents in certain activities and installations [6]. The new rules harmonize the previous standards 2004/42/EC and Regulations (EC) No 765/2008 and (EU) No 305/2011 [7], limiting the emission of DMF from 20 mg/Nm³ to 2 mg/Nm³.

Nm³ indicates the so-called "normal cubic meter" i.e. the volume of gas that occupies a cubic meter when this gas is at a temperature of 15 degrees Celsius and a pressure of 1.013 bar. The plant costs to be handled by textile small and medium-sized enterprises for the reduction of DMF emissions are therefore significantly high and often disproportionate to the actual quality improvement of the realized product.

Consequently, in this textile field there is an urgent need in devising methods to reduce the use of Dimethylformamide for the manufacturing of artificial leather-based products.

Accordingly, the aim of this work is to improve the state of the art in the production of leather-like fabrics through the development of an innovative process of coagulation of polyurethane in aqueous solution for replacing the current highly polluting process that involves the use of DMF. This will make it possible to obtain a product with technical characteristics close to the ones characterizing conventional leather-like products, but fully eco-friendly in nature. With this new process, the polyurethane dispersion is foamed in a watery solution to obtain a wide-ranging product (e.g. artificial leather, cleaning cloth, technical waterrepellent and thermo-insulating fabrics) with appropriate aesthetic and structural characteristics. The devised process involves the use of an infrared (IR) thermo-coagulation process, which avoids a structural collapse of the foam.

Therefore, a further innovation of the work is the development of a system that allows the layer of polyurethane foam to maintain much of the initial volume giving the finished product the honeycomb layer that gives the desired characteristics. This is possible using a thermo-coagulant, i.e. a coagulant activated (at the right time) by means of an infrared field. This will avoid the use of a strong electrolyte in the dispersion that would allow the coagulation, but would also ruin the dispersion making it practically inoperative.

Tab. 1 Technical requirements for leather-like products

2 Materials and methods

As mentioned above, the main aim of the proposed system is to disperse and foam the polyurethane to be layered on the textile substrate by using an aqueous solution to obtain a variegated product (synthetic leather, cleaning cloth, water repellent fabric, insulation fabric, etc.) characterized by appropriate aesthetical and structural features. A thermo-coagulation process, based on the application of IR emissions, allows maintaining much of the initial volume of the polyurethane foam thus providing the finished product a leather-like layer. Such a process is able to confer to the final product the desired characteristics without using a strong electrolyte in the dispersion. Accordingly, the main tasks of the project are:

- 1.Design and production of optimal raw supports to be coated
- 2.Design and production of optimal raw supports for the coating process
- 3. Coagulation of the PU dispersion, avoiding the use of DMF
 - 4. Finishing and testing of coated fabrics

Prior to describe the new process, it is necessary to state a number of technical requirements based on the typical performance of leather-like products. In detail, artificial leather fabrics are required to meet a number of technical requirements both for the substrate and for the coated finished fabric [8]. Tab.1 lists such requirements.

| | Parameter | Target value | |
|-----------------------|---|---------------------|--|
| | Color fastness to artificial light (test method ISO 105-B02/94) with blue scale and range from 1 to 8 [9] | 7-8 | |
| | Color fastness with gray scale range from 1 to 5 [9] | 5 | |
| | Color fastness to perspiration (test method ISO 105- | 5 acidic | |
| | E04/94) with gray scale range 1 to 5 [10] | 5 alkaline | |
| Substrate Parameters | Color fastness to washing (test method 105-C10:2006) | 5 | |
| | with gray scale range from 1 to 5 [11] | J | |
| | Color fastness to rubbing (test method ISO 105X12/01) | 5 acidic | |
| | with gray scale range from 1 to 5 [12] | 5 alkaline | |
| | Color fastness to washing in water (test method ISO | 5 | |
| | 105-E01/94) with gray scale range 1 to 5 [13] | 3 | |
| | Thermal resistance [14] | 0.020 - 0.030 W/mK | |
| Coated fabric Parame- | Dimensional stability [15] | 0.5% - 3.0% | |
| ters | Resistance to abrasion [16] | 250 g/cm2 | |
| | Mean tensile stress [17] | >118 N | |
| | Elongation [17] | >2% | |

2.1 Design and production of optimal raw supports to be coated

A collection of 10 different types of fabrics (see Tab.2) each distinguished by a different blend (i.e. different composition) has been developed as a support material for the polyurethane coating process to improve the proposed process. As one of the main goals

of the project is to make fabrics as environmentally friendly as possible, the blends are ideally made of cotton blended with low polyester (for technical fabrics) or linen/cotton percentages (for fabrics to be used in clothing and handbags).

Tab. 2 Fabrics used as a support for the coating process

| Fabric Name | Composition | Warp wires (N°/cm) | Warp count (m/g) | Weft wires (N°/cm) | Weft count (m/g) | Fabric linear Weight (g/m) | Fabric Height (cm) |
|----------------------|------------------------------|--------------------------|------------------------|--------------------------|------------------------|-------------------------------------|--------------------------|
| Kos Wash | 100% cotton | 44 | 11.8 | 25 | 16 | 375 | 160 |
| Cover Cot | 100% cotton | 85 | 29.6 | 41 | 60/1 | 230 | 160 |
| Scamosciato | 94% cotton 6% poly- ester | 23 | 9.5 | 39 | 12 | 530 | 178 |
| Stuoia fiam- mata | 100% cotton | 32 | 7.1 | 12 | 5.4 | 500 | 160 |
| Popeline 50/50 | 100% cotton | 57 | 29.6 | 32 | 50/1 | 185 | 160 |
| Nattè Ecolog- ico | 55% linen, 45% cotton | 40 | 11.8 | 26 | 26 | 360 | 160 |
| Twill Ecologico | 55% linen, 45% cotton | 40 | 11.8 | 25 | 26 | 350 | 160 |
| Linone | 100% linen | 21 | 8.9 | 16 | 1/15 | 415 | 162 |
| Tela Lino | 100% linen | 20 | 19.5 | 23 | 39 | 200 | 160 |
| Drill Cotone | 100% cotton | 52 | 11.8 | 22 | 20 | 405 | 160 |

2.2 Design and production of optimal raw supports for the coating process

Before the support undergoes the innovative coating process a series of treatments are required. First, the fibers emerging from the fabric surface are burned by sliding the fabric, tangentially, under a flame (gasair mixture varying in the range 30-35% and flame temperature equal to about 950 °C) with a speed of 80

m/min. Setting parameters used for the burning process are in Tab. 3.

Afterwards, the fabric is processed by means of an enzymatic desizing with amylases, washed using an industrial washing machine and whitened by bleaching soda treatments. Finally, the fabric is dried into a stenter with a working temperature of 120/130°C and then pre-shrunk.

Tab. 3 Burning process parameters

| Parameter | Settings |
|--|----------------|
| Distance of the fabric from the visible flame tip | 2-3 mm |
| Fabric flow speed | 80 m/min |
| Air-gas mixture | 30-35% |
| Type of burn | Tangential |
| Value of Be (Baumé) degrees [7] | 18 °Be |
| Cotton-based concentration values | 30 °Be at 14°C |
| Concentration values of cotton rayon viscose blend | 14 °Be at 20°C |

Tab. 4 Textile substrate parameters

| Parameter | Measured Value | Delta [%] |
|---|----------------|-----------|
| Color fastness to artificial light (test method ISO 105-B02/94) with blue | | 0-6% |
| scale and range from 1 to 8 | / | 0-0 / 0 |
| Color fastness with gray scale range from 1 to 5 | 5 | 0% |
| Color fastness to perspiration (test method ISO 105-E04/94) with gray | 5 acidic | 5% |
| scale range 1 to 5 | 4.5 alkaline | 3 / 0 |
| Color fastness to washing (test method ISO 105-C01/89) with gray scale | 5 | 0% |
| range from 1 to 5 | 7 | 070 |
| Color fastness to rubbing (test method ISO 105X12/01) with gray scale | Moist 4.5 | 5% |
| range from 1 to 5 | Dry 5 | 3 / 0 |
| Color fastness to washing in water (test method ISO 105-E01/94) with | 4.5 | 10% |
| gray scale range 1 to 5 | 7.3 | 10/0 |

The technical characteristics of the manufactured supports are assessed through a series of laboratory tests to assess their compliance with the expected technical requirements. Results of the experimental characterization, listed in Tab. 3, demonstrated that the textile substrate is adequate for the subsequent coating process since its properties are in-line with the values for similar substrates typically used for leatherlike products (target value in Tab. 4).

2.3 Coating process

Polyurethanes in aqueous dispersion are available on the market [18], but the main obstacle to their use in artificial leather coating processes is their high stability, so that the normal coagulants, used for other types of dispersion, did not allow obtaining the desired result in the desired time. To overcome these issues, it was necessary to perform the following preliminary steps:

Tab. 5 Witcobond 374-13 properties

a) Selection of a category of polyurethane that allows an aqueous dispersion according to the physical characteristics of resilience, elasticity, rigidity, flexibility, transparency, colour and elongation at break. Among the several available polyurethane typologies, the Witcobond 374-13 [19], an aliphatic polyester anionic polyurethane dispersion with no free isocyanate, proved to be the most effective in terms of resilience, transparency and resistance. Its properties are in Tab. 5.

| Parameter | Value |
|------------------------------|-------------------------------|
| Solids Content (%) | 59 – 61 |
| pH at 25°C | 7-9 |
| Viscosity at 25°C (mPa • s) | 50-400 |
| Polyurethane Dispersion Type | Aliphatic, polyester, anionic |
| Specific Gravity at 25°C | 1.07 |

b) Selection of mineral or vegetal filler, of foaming surfactants and crosslinking agents. The addition of a mineral or vegetal filler, by increasing the solid content (i.e., the concentration of dispersed and/or dissolved solid material in the polyurethane -water mixing) promotes the coagulation; however, too much mineral filler cannot be used because it alters the characteristics of the final product. Therefore, to sufficiently unstabilize the polyurethane in aqueous dispersion, at least one Cobalt sulfide (CoS) is added. As widely recognized, CoS is a non-volatile organic compound (with a melting point greater than 125°C), whose solubility is greater than 1000 g/l at 20°C. Among the many compounds suitable for this purpose, sucrose is preferred because of its high availability at low cost and/or low environmental impact. The CoS, by increasing the dry concentration, facilitates the subsequent coagulation of PU and, given its high solubility, during the various washings to which the semi-finished composite material is subjected, it is removed from the coagulated layer, resulting in the formation of a microporous structure. In addition to the coagulant, an acid dissociating compound is also used. It consists of a salt with high ionic dissociation in water and capable of producing a pH decrease to values between 3 and 6 when subjected to temperatures greater than 100°C. Ammonium salts such as NH4Cl or (NH4)2SO4 can be used for this purpose. The mix is completed by adding foaming surfactants such as sodium sulfosuccinate, sodium lauryl sulfate, sodium oleate, potassium oleate, ammonium stearate, or their mixtures. For the devised process, they are added to the mixture at a mass fraction ranging from 2.5 to 5 wt%. Finally, crosslinking agents are added to the mixture. In the devised system, melamine/formaldehyde resins, carbodiimides, polyacrylamide resins, epoxy resins can be used. Melamine/formaldehyde resins are preferred and

commercially available and therefore represent the best choice; the used amounts is equal to a mass fraction of 3 wt% (percentage by weight) of the total mixture. Once the compound is created with the proper mix of elements, it is possible to process it. The first process, carried out by using a micronizer (see Figure 1) consists of reducing its granulometry size from the initial 300-400 μm to 30-70 μm , which is a more appropriate size for performing the subsequent coating process.

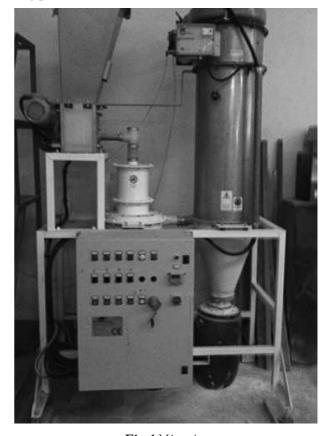


Fig.1 Micronizer

The micronized powder is then sent to a foaming machine (depicted in Fig. 2) together with water and air. The foaming machine has been appositely devised to obtain a foam with a density of 120 g/l. It consists

of cylinder (volume equal to 0.254 m3) equipped with water and air inlet channels and a rotating auger to produce foam.



Fig.2 Foaming machine

The weight of the PU and added products is equal to 50 kg with a density of 200 kg/m³. On the basis of technicians knowledge, the foam is required to have a density of around 205 g/l and the expected expansion coefficient is equal to 1.1:1. To this aim, the foam is required to be composed by about 8% of air. Therefore, the main issue is to detect the optimal rotational speed of the auger to obtain the desired foam density. First, it is necessary to evaluate the optimal inlet air pressure to be sent into the cylinder. Tests were performed by varying the pressure in the range 1-6 bar, with a step equal to 0.5 bar and constant rotational speed equal to 31.5 rad/s and airflow equal to 30 g/s.

Results (see Fig. 3a) of an interpolation of measured data shows that the higher percentage of air absorbed by the mixture (i.e. 7%) can be obtained when the pressure is equal to 3.2 Bar. Good results are also achievable using a pressure varying in the range 3-3.5 bar. In this work, a 3 bar pressure was selected. Therefore, using air at such a pressure, the rotational speed was varied in the range 15.8 – 68 rad/s with a step equal to 5.3 rad/s. Finally, as depicted in Fig. 3b, the optimal rotational speed for obtaining a quantity of air equal to 8% of air is equal to roughly 34.8 rad/s. The mixing process, which allows mixing 0.236 m³ of PU (plus additive materials) with 0.088 m³ of air, lasts 2 min. The obtained foam density is equal to 204.4 g/l and the expansion coefficient is 1.08:1.

Subsequently, the mixture polyurethane-water feeds a blade coating machine (see Fig. 4a) by means of a flexible pipe. This machine allows the support coating by providing a uniform layer (2 mm thickness) of polyurethane. It is important to highlight that, despite the special composition of the mixture, the

above described process still does not allow a proper coagulation without the use of DMF. Moreover, although the polyurethane coagulates (with an extremely "slow" chemical process) the coating is water-soluble and so it may results unsuitable for technical applications.

Accordingly, in order to consolidate the coagulation, the coated fabric passes through a stenter equipped with IR lamps (Fig. 4b). The infrared illumination affords both the coating drying and a polymerization thus providing an "indissoluble" grid. In particular, the coated fabric enters under a distributor of powders where it receives 30-40 gr/m of sodium sulfate with a particle size between 30 and 70 μm ; then, the semi-finished product passes under a 6 m long area where IR lamps are placed in order to allow a first coagulation. The fabric crosses the IR-illuminated area for 40 s, therefore the fabric has a linear speed equal to 10 m/s. For this particular application, IR lamps with 0.35W/mm of maximum density of nominal power are used. Radiation peak of the lamps is in the range $2.2 - 3.2 \,\mu m$ which is particularly suitable for the fast heating of surface parts or thin thickness materials.

Afterwards, the fabrics processed with a stenter where the final coagulation, together with drying and cross-linking of the polymer, take place. Temperature in the stenter is maintained equal to 150°C for the entire process. Drying duration is equal to 120 s while reticulation lasts 60 s.

Eventually, the fabric is wrapped on a roller. Once the new type of coated fabrics manufactured, it is washed in order to remove possible impurities. This phase, carried out by using a washing machine (see Fig. 5a), allows to eliminate surfactants, sucrose and sodium sulfate. After washing, the fabric is dried again and further processing such as printing and embossing can be made. Fig. 5b shows some examples of obtained leather-like fabrics.

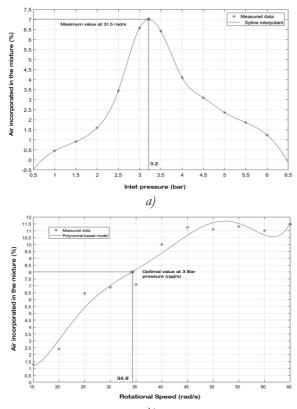


Fig. 3 a) air incorporated in the mixture vs. Inlet pressure at 300 RPM rotational speed; b) air incorporated in the mixture vs. Rotational speed at 3 Bar pressure.



a)

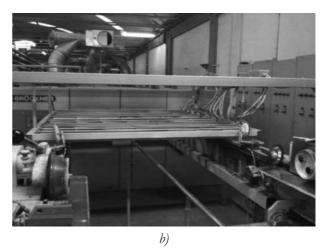


Fig. 4 a) blade coating machine; b) stenter equipped with IR lamps.





Fig. 5 a) Washing machine; b) some examples of leather-like products obtained by means of the devised system

3 Results

Ten prototypes, one for each substrate depicted in Tab. 2 were manufactured with the developed system. These were tested to verify their actual compliance with the technical requirements typically stated for artificial leather products. In detail, the following tests have been carried out to prove the effectiveness of the prototypes created using the DMF-free process.

3.1 Thermal resistance

Thermal resistance R is the ratio between the absolute temperature difference ΔT between the two faces of the insulating material (i.e. the fabric) and the amount of thermal energy transferred in the unit of time (thermal flow ϕ) through the unit of surface d [20]. Thermal resistance in fabrics can be measured in W/m·K This parameter is certainly one of the most interesting for the coated fabrics manufactured with the new method. Tested specimens proved to have similar characteristics with respect to typical leatherlike coated fabrics, as shown in Tab. 6 (showed results are related to four up to the ten prototypes, namely Kos Wash, Cover Cot, Scamosciato and Stuoia fiammata). For all the prototypes, the mean value of thermal resistance is 0.030 W/m·K with a standard deviation equal to 0.005.

3.2 Dimensional Stability

As required by UNI EN 1606:2013 standard, the

new polyurethane formulation should undergo a dimensional stability test consisting of the determination of the increase in deformation of a foam specimen kept under a constant load, under specific conditions of temperature, humidity and time [21]. The purpose of the test is to define an admissible load for a practical application of the insulating material by evaluating its long-term behavior. Under operating conditions with constant loads within 10-15 % of the compressive strength, the percentage deformations of the thickness are kept within irrelevant values (less than 2%) for all specimens, as depicted in Tab. 6 for the four above considered prototypes. For the whole set of prototypes the mean value of dimensional stability results equal to 2.52% with a standard deviation equal to 0.56.

3.3 Resistance to abrasion

It is necessary to test the various polyurethane-coated surfaces for resistance to abrasion caused by brushes, sponges, or other materials. Abrasion tools that produce micro-damage on the surfaces by repeated rubbing and scraping under controlled conditions optimally simulate the daily conditions of wear and tear. The Branca abrasion test [22] is carried out by subjecting a test sample to the action of a nylon brush under the pressure of a specified weight and a specified number of alternating cycles. Results of test for the four considered test cases are in Tab. 6. For the whole set of prototypes the mean value of this parameter results equal to 256.5 g/cm² with a standard deviation equal to 47.5.

Tab. 6 Thermal resistance, Dimensional stability and resistance to abrasion

| Prototype | Thermal resistance | Dimensional stability | Resistance to abrasion |
|-----------------|--------------------|-----------------------|------------------------|
| Kos Wash | 0.025 W/m·K | 2.0% | 300 g/cm ² |
| Cover Cot | 0.027 W/m·K | 1.5% | 270 g/cm ² |
| Scamosciato | 0.032 W/m·K | 2.5% | 280 g/cm ² |
| Stuoia fiammata | 0.035 W/m·K | 3.0% | 250 g/cm ² |

3.4 Mechanical strength

Tensile strength of a yarn or fabric is defined as a maximum load that it will endure without breaking when subjected to uniaxial tensile loading [23]. In this work, mechanical strength is measured according to ASTM D5034 standard [17]. Results for the four selected prototypes are in Tab 7. For the whole set of prototypes the mean value of this parameter results equal to 61.1 N with a standard deviation equal to 18.5.

4 Conclusions

Today, sustainable development and reduction of the environmental impact are issues that textile companies have to take into account in order to remain competitive in the future market since they represent a key issue for further development of innovative products. In particular, there is today a change in attitude that involves a transition from the concept of "environment as an issue" to the one of "environment as a possibility" [24]. With the proposed method, it is possible to produce eco-compatible avoiding the use of DMF and resulting in new ecological fabrics characterized by a very high quality. The results showed that the performance of all prototypes made with the new system is comparable to that of those made with the traditional method. The process, involving both the use of a number of compounds used to facilitate the coagulation of the aqueous solution of PU and the use of IR for accelerating the coating procedure [25] involves a higher cost, when compared to a similar traditional facility, estimated at 2% more. This cost is mainly due to the slight increase of energetic costs to keep IR lamps operative during the entire coagulation process. The new process, on the other hand, has the

significant advantage of not requiring DMF. Therefore, since on the Company that tested the process an entire production line, out of four, has been converted to this new process, there is a 25% saving in the emission of this compound into the wastewater to be treated and a similar reduction in emissions into the atmosphere.

Tab. 7 Mechanical Strength

| Fabric name | Fabric image after tensile test | Stress-strain curve | Mean value of tensile stress (N) | Elonga- tion % |
|----------------------|---------------------------------|---|--|-------------------|
| Kos Wash | | Force (hgf) | 114.6 | 6.33 |
| Cover Cot | | Force (kgf) | 193.6 | 6.89 |
| Scamosciato | | Force (kgf) | 249.2 | 2.38 |
| Stuoia fiam- mata | | Force (kgf) 10 20 21 22 23 24 25 26 27 28 28 29 20 20 20 20 20 20 20 20 20 | 262.4 | 8.38 |

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